

## 3. Geologic and Hydrologic Setting

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This section provides information on the geologic and hydrologic setting, and beneficial land and groundwater use within the study area.

### 3.1 Tectonic Setting

Oregon and Washington are located on the North American continent crustal plate. The continental plate boundary is convergent with the Juan de Fuca oceanic crustal plate and forms the Cascadia Subduction Zone. The oblique convergence of the North American Plate with the Juan de Fuca Plate has created northwest-trending fault zones and crustal blocks (Baldwin 1976). These structural features govern the geologic and hydrologic setting of the Portland Basin.

The Portland Basin, a north-west trending structural basin, encompasses approximately 1,310 square miles and is characterized by relatively low topographic relief with areas of buttes and valleys containing steep slopes (McFarland and Morgan 1996). The basin is bordered on the east by the foothills of the Cascade Mountains, on the west by the Tualatin Mountains, on the south by the Clackamas River, and on the north by the Lewis River.

### 3.2 Topography

The Columbia River dominates the topography of the study area. The project corridor lies within the Columbia River main valley, with the exception of a small area north of the SR 500 interchange that is located in the Burnt Bridge Creek watershed (Exhibit 1-1). Burnt Bridge Creek flows into Vancouver Lake before discharging to the Columbia River. Project area elevations vary from approximately 10 feet in the Columbia River floodplain to about 220 feet at the drainage divide between the Columbia River and Burnt Bridge Creek valleys.

### 3.3 Fluvial Setting

The Columbia River drains almost 220,000 square miles in seven states and Canada with land in forest, agricultural, residential, urban, and industrial uses. The Lower Columbia River, that section of the river most pertinent to the impact analysis, flows from Bonneville Dam at River Mile 146 to the mouth of the river, and drains an area of 18,000 square miles. Adjacent to the study area, Hayden Island divides the mainstem of the Columbia River, which flows to its north, from a side channel called the North Portland Harbor, which flows to its south. The I-5 highway crosses both channels near River Mile 106.5.

1 Exhibit 3-1 displays Columbia River bathymetry within the study area. The figure  
2 indicates that depth of in-water sediments in the study area extends from the ordinary  
3 high water line<sup>3</sup> at 21.2 feet North American Vertical Datum 1988 (NAVD 88) to a  
4 depth of approximately -25 feet NAVD 88. Geotechnical borings and bathometric  
5 surveys completed within the footprint of the proposed crossing indicate that the depth to  
6 the bottom of unconsolidated sediments (alluvial and/or catastrophic flood deposits) in  
7 the study area ranges from -40 to -230 feet NAVD 88 (DEA 2006) (Shannon and Wilson  
8 2008). Underlying these sediments is the top of the Troutdale Formation.

9 The top layer of river substrate is composed of loose to very dense alluvium (primarily  
10 sand and some fines), underlain by approximately 20 feet of dense gravel, underlain by  
11 the Troutdale Formation. Additional information regarding the characteristics of in-water  
12 sediment material in proximity to the study area is currently being compiled by the U.S.  
13 Army Corps of Engineers (USACE). This 2008 evaluation report should be open for  
14 public review sometime this summer (Siipola, April 4, 2009).

15 Burnt Bridge Creek defines the northern boundary of the study area. The creek originates  
16 in East Vancouver from field ditches that drain a large wetland area between NE 112th  
17 Avenue and NE 164th Avenue. The creek is approximately 12.9 miles in length and  
18 alternates between ditches and natural channels. Except for floodplains, parks, and  
19 wetlands, nearly the entire basin is urbanized. In the project area, the creek flows through  
20 a small canyon with a narrow floodplain. The creek passes under the existing highway in  
21 a culvert north of the project area.

## 22 **3.4 Stormwater**

### 23 **3.4.1 Existing Stormwater Drainage System**

24 The existing stormwater drainage systems in the study area are comprised of closed  
25 conveyance systems that discharge runoff to either the Columbia River or Burnt Bridge  
26 Creek Watersheds. These watersheds are highly urbanized within the study area. The  
27 existing drainage systems are described below based on their receiving waterbody.

#### 28 ***Columbia River Watershed***

29 The total drainage area included in the analyses of stormwater draining to the Columbia  
30 River Watershed is about 486 acres. Of this area, approximately 204 acres (or about 42  
31 percent) is comprised of impervious surfaces that include highway, streets, parking lots  
32 and alleys. The area extends north from the Columbia River to just south of SR 500. The  
33 drainage area includes I-5, the western end of SR 14, and downtown Vancouver. With the  
34 exception of SR 14, runoff from this drainage area receives no water quality treatment  
35 prior to being released to the Columbia River. Runoff from the eastbound lanes of SR 14  
36 (about 3 acres) sheds to the shoulder where it disperses and/or infiltrates to groundwater.

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<sup>3</sup> The point on a stream bank to which the presence and action of surface water is so continuous as to leave a district marked by erosion; destruction or prevention of woody terrestrial vegetation; predominance of aquatic vegetation; or other easily recognized characteristics.

1 Runoff from Interstate Bridge drains directly from the bridge decks through scuppers to  
2 the Columbia River or ground below. North of the Columbia River, conveyance systems  
3 collect runoff from I-5, SR-14 and streets in downtown Vancouver. The runoff is  
4 discharged directly to the river via several outfalls located from about ½ mile east  
5 (upstream) of the existing bridges to about ½ mile west. Over 80 percent of the total  
6 drainage area is served by a single conveyance system that discharges to the Columbia  
7 via a 60-inch diameter outfall located immediately east of the Interstate Bridge. Runoff  
8 also discharges to the Columbia River via several outfalls located in the immediate  
9 vicinity of the existing I-5 bridges (see Exhibit 3-1) (Clark County 2005).

10 ***Burnt Bridge Creek Watershed***

11 The total drainage area included in the analyses of stormwater draining to Burnt Bridge  
12 Creek is about 190 acres, of which approximately 86 acres (or about 45 percent)  
13 comprises highway, streets, parking lots and alleys. The area includes SR 500, the I-5/SR  
14 500 interchange, I-5 north of the interchange, and adjacent neighborhoods. Runoff from  
15 approximately 66 acres of impervious surface is directed to an infiltration pond located  
16 immediately south of the I-5/Main Street interchange. Runoff from the remaining area  
17 flows to wet pond located east of the I-5/SR 500 interchange.



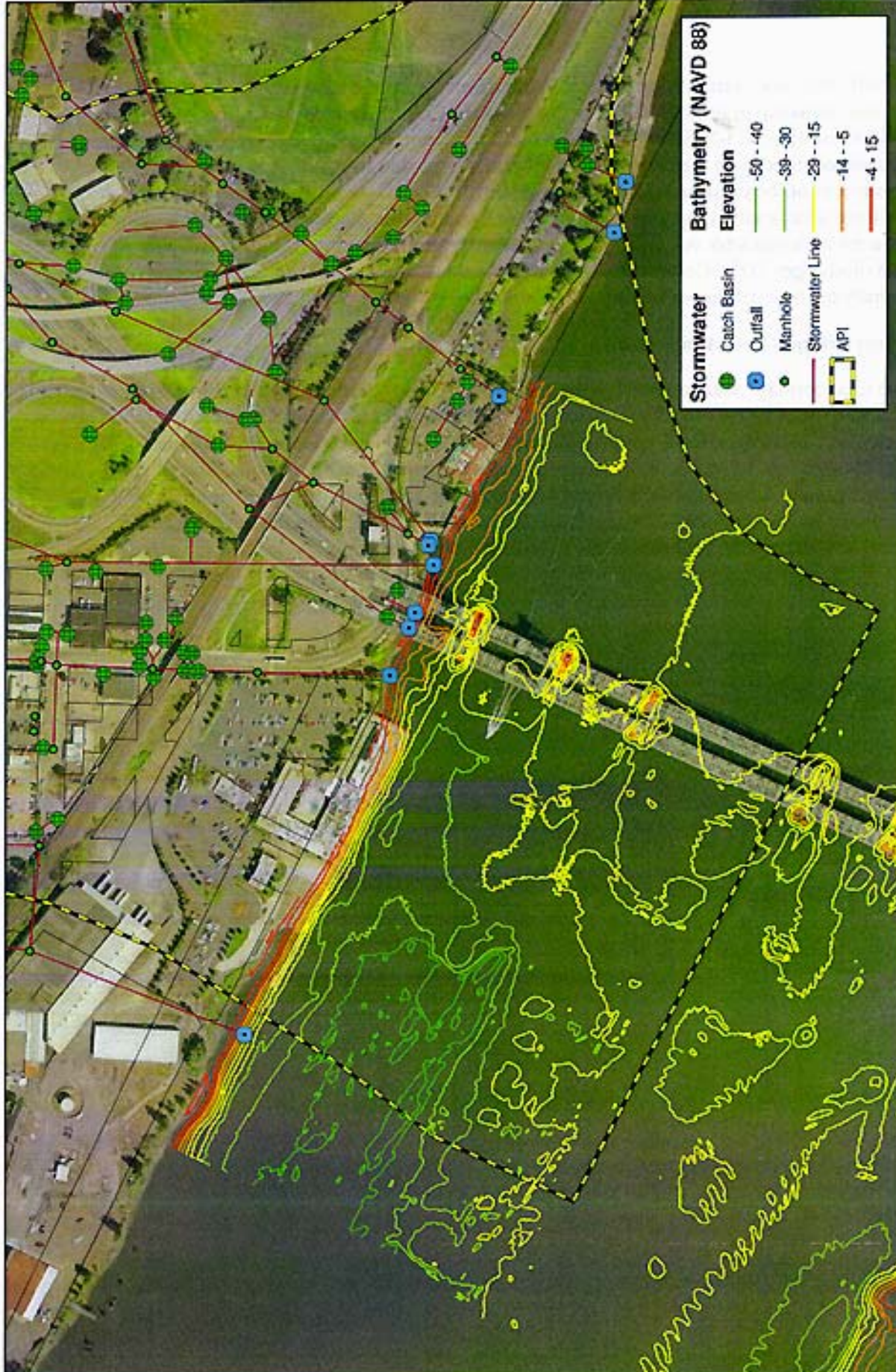
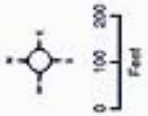


Exhibit 3-1: Columbia River  
 Bathymetry Map  
 Troutdale SSA Evaluation  
 Columbia River  
**CROSSING**



## 3.5 Geologic Units

Geologically recent deposits that fill in the Portland Basin consist of conglomerate, gravel, sand, silt, and some clay from volcanic, fluvial, and lacustrine material (Pratt et al. 2001). Late Pleistocene catastrophic flood deposits cover much of the surface within the study area. Deposits originating from an ancestral Columbia River underlie the catastrophic flood deposits. These sedimentary deposits overlie Miocene basalt flows of the Columbia River Basalt Group (Swanson et al. 1993). The Columbia River Basalt Group overlies lava flows and volcanic breccias of Oligocene age.

Geologic units within the study area are described below by increasing age. The spatial distribution of surficial geologic units is presented on Exhibit 3-2.

### 3.5.1 Artificial Fill (Qaf)

Artificial fill material was used to modify existing topographic relief and typically consists of sand, silt, and clay with some gravel and debris. Fill areas mapped with inferred contacts represent lakes and marshes that may have been drained rather than filled. Fill 5 to 15 feet thick is common in developed areas of the Willamette River and Columbia River floodplains (Madin, 1994). However, thickness and distribution are highly variable (Beeson et al. 1991).

### 3.5.2 Alluvium (Qal)

Alluvial deposits include material derived from present day streams and rivers, their floodplains, and abandoned channels. The alluvial deposits are typically Holocene to upper Pleistocene in age. Alluvial material consists of unconsolidated gravel, medium to fine sand, silt, and organic-rich clay. Cobble-sized material may be present within existing or abandoned stream channels. Thickness is typically less than 45 feet, but may be up to 150 feet thick locally. Alluvium is exposed at the surface from just south of the Columbia Slough in Oregon to approximately ¼ mile north of the Columbia River in Washington (Beeson et al. 1991; Phillips 1987).

### 3.5.3 Catastrophic Flood Deposits (Qff/Qfc)

The catastrophic flood deposits resulting from the Pleistocene-aged Missoula Floods are derived from the repeated failure of ice dams located on the Clark Fork River in northwestern Montana (Bretz and others 1956). Glacial Lake Missoula was created by ice dams from the advancing front of the Purcell Trench lobe of the Cordilleran ice sheet. The floods released approximately 500 cubic miles of water, flooding portions of eastern Washington, the Columbia Gorge, and the northern Willamette Valley (Bretz et al. 1956; Allen et al. 1986). The flooding occurred at least 40 times during the Pleistocene (16,000 to 12,000 years ago), depositing boulders, cobbles, gravel, sand, and silt (Waitt 1985). The flood waters would be impounded by valley constriction south of Kelso and backup to elevations as much as 350 feet mean sea level (msl). As flood water velocities were reduced, sediment loads were deposited in foreset bedded gravel and sand similar to delta deposition (Robinson, Noble and Carr 1980).



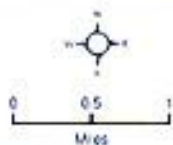
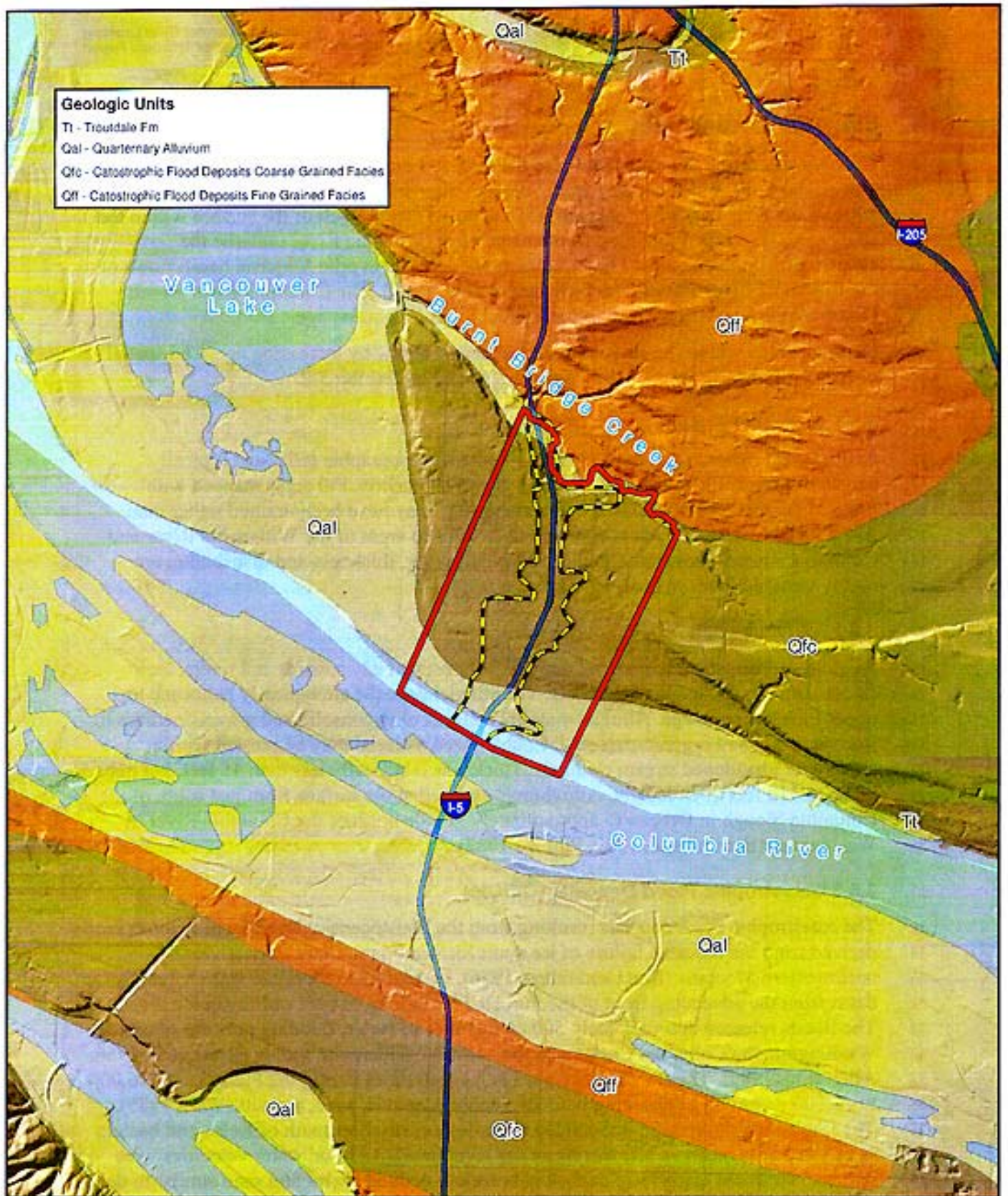


Exhibit 3-2: Geologic Units  
Location Map  
Troutdale SSA Evaluation



1 This deposit is subdivided into two facies by Madin (1994): a fine-grained facies (Qff)  
2 and coarse-grained facies (Qfc). Both are present locally. The finer sediments consist of  
3 primarily coarse sand to silt. The fine sand and silt is composed of quartz and feldspar  
4 with white mica. The coarser sand is composed primarily of basalt. The coarse-grained  
5 facies (Qfc) consists of pebble to boulder gravel with a coarse sand to silt matrix.

#### 6 **3.5.4 Troutdale Formation (Tt)**

7 The Troutdale Formation (Miocene to Pliocene in age) underlies the catastrophic flood  
8 deposits and consists of coarse- to fine-grained fluvial sedimentary rock derived from the  
9 ancestral Columbia River. The unit is a friable to moderately strong conglomerate with  
10 minor sandstone, siltstone, and mudstone. Pebbles and cobbles are composed of  
11 Columbia River Basalt (described below), exotic volcanic, metamorphic, and plutonic  
12 rocks. The matrix and interbeds are composed of feldspathic, quartzo-micaceous, and  
13 volcanic lithic and vitric sediments. The formation exhibits cementation mantling on  
14 some of the grains (Beeson et al. 1991).

#### 15 **3.5.5 Sandy River Mudstone (Tsr)**

16 The Sandy River Mudstone (Pliocene in age) underlies the Troutdale Formation and  
17 consists of fine-grained, predominantly fluvial and minor lacustrine sediments. The unit  
18 is a friable to moderately strong sandstone, siltstone, and claystone. The mudstone is  
19 composed of primarily quartz-feldspathic and white mica sediments (Beeson et al. 1991).

#### 20 **3.5.6 Miocene and Older Rocks**

21 The Columbia River Basalt Group (CRBG) (late Miocene and early Pliocene in age)  
22 consists of numerous basaltic lava flows which cover approximately 63,000 square miles  
23 and extend to thicknesses greater than 6,000 feet. The CRBG is composed of dark gray to  
24 black, dense, crystalline basalt and minor interbedded pyroclastic material. Beneath the  
25 CRBG are upper Eocene to lower Miocene volcanic and marine sedimentary rocks. The  
26 volcanic rocks typically consist of altered basalt, basaltic andesite, and pyroclastic rocks.  
27 The marine sedimentary rocks typically consist of fossiliferous tuffaceous shale and  
28 sandstone with minor conglomerate lenses (Madin 1994).

### 29 **3.6 Hydrogeologic Setting**

30 As the geologic units described above were deposited in the deforming Portland Basin,  
31 hydrogeologic units were also formed. The physical nature and depositional environment  
32 of the geologic material will create units of material that possess dissimilar hydraulic  
33 properties. Groundwater moving through the material will travel at different rates  
34 depending on the physical properties of the hydrogeologic unit. The physical properties  
35 of units in the TSSA are further discussed below.

1 The 1993 United States Geologic Survey (USGS) (Swanson et al. 1993) report describes  
2 eight major hydrogeologic units in the Portland Basin (Exhibit 3-3). These units are, from  
3 youngest to oldest and increasing depth:

- 4 • Unconsolidated Sedimentary Aquifer (USA)
- 5 • Troutdale Gravel Aquifer (TGA)
- 6 • Confining Unit 1 (CU 1)
- 7 • Troutdale Sandstone Aquifer (TSA)
- 8 • Confining Unit 2 (CU 2)
- 9 • Sand and Gravel Aquifer (SGA)
- 10 • Older Rocks

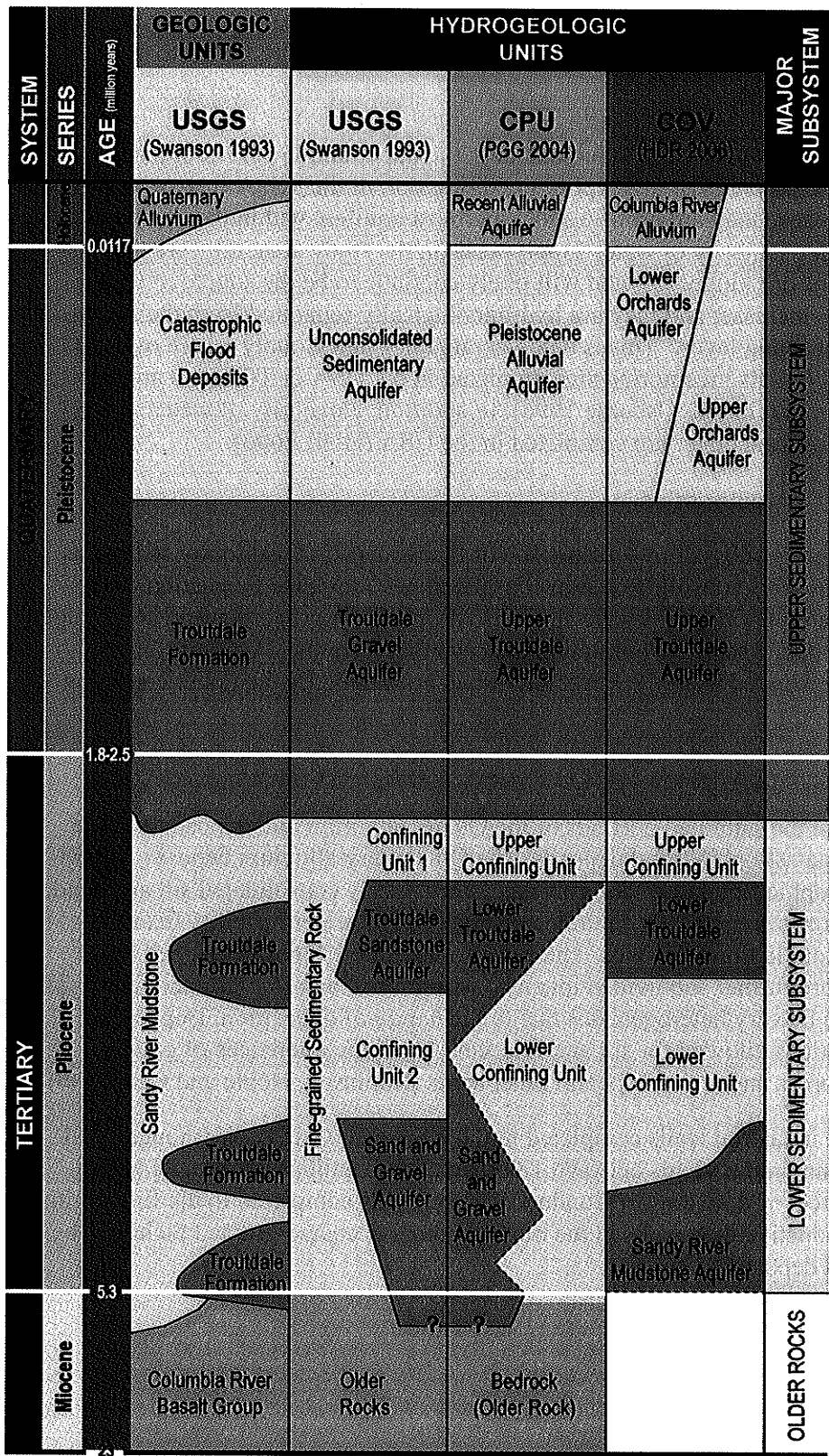
11 The eighth unit is referred to as undifferentiated fine-grained sediments where the TSA  
12 and the SGA appear to have pinched out or there is insufficient information to  
13 characterize the aquifer units within the fine-grained Sandy River Mudstone. Where this  
14 occurs, CU 1 and CU 2 cannot be separated and have been mapped as undifferentiated  
15 fine-grained sediments. The older rocks, consisting of older volcanic and marine  
16 sedimentary rocks of generally low permeability, are present at depths estimated to range  
17 up to 1,600 feet in the central area of the basin. They are poor aquifers and too deep to be  
18 used as a primary source of water in the site region. Due to these conditions, no further  
19 discussion is presented regarding the older rock unit.

20 The Portland Basin aquifer system has also been grouped into three major subsystems:

- 21 • Upper sedimentary subsystem (USA and TGA)
- 22 • Lower sedimentary subsystem (CU 1, TSA, CU 2, and SGA)
- 23 • Older rocks

24 This grouping is based on regionally continuous contacts between units of different  
25 lithologic and hydrogeologic characteristics (Swanson et al. 1993). Exhibit 3-3 presents  
26 other nomenclatures used to describe the hydrogeologic units by Clark Public Utilities  
27 (CPU) and the City of Vancouver (COV). For the purpose of consistency with EPA's  
28 (2006) determination, terminology used by McFarland and Morgan (1996) which was  
29 derived from Swanson and others (1993) will be presented in this report.





**Exhibit 3-3**  
**Geologic Units and**  
**Comparison of Hydrogeologic**  
**Unit Terminology**

Troutdale SSA Evaluation

## 3.7 USA and TGA

The EPA (2006) defines the TSSA to include both the upper and lower sedimentary subsystems. For the purposes of this report, the discussion of the TSSA focuses on the USA and TGA because they are prolific and uppermost aquifers within the Portland Basin; they contain a majority of water supply wells in the study area; they are the primary aquifers for drinking water and will likely continue to be the source of water supply as demands increase; and they are hydrogeologically separated from the lower subsystem by a confining layer.<sup>4</sup> This is demonstrated in Clark County where over 90 percent of the 7,111 wells inventoried are completed in the USA or TGA and are less than 300 feet in depth (Gray & Osborne 1996). In addition, a majority of water supply wells for the City of Vancouver are completed in the USA (HDR 2006).

### 3.7.1 Hydrologic Characteristics

The upper sedimentary subsystem is composed of Pleistocene to Quaternary sediments and consolidated to semi-consolidated gravel of the upper Troutdale Formation. The Pleistocene to Quaternary deposits have similar hydrogeologic properties and are grouped as the USA. The upper Troutdale Formation deposits that form the TGA are hydrogeologically isolated from the lower Troutdale Formation by the upper confining unit (CU1).

#### USA

The USA occurs in the saturated portions of the Quaternary alluvium deposits and the Pleistocene-aged catastrophic flood deposits. The Quaternary alluvium deposits, which overlie the catastrophic flood deposits, consist of very poorly consolidated silt and sand. The alluvium deposits are partially saturated and have a lower permeability than the underlying catastrophic flood deposits. The catastrophic flood deposits mapped by Phillips (1987) were further subdivided into a coarse-grained and fine-grained facies. The flood deposits can be very heterogeneous due to the nature of deposition. Deposition under flood conditions allowed for silt and fine sand to fill the interstices of gravel deposits in some areas and remain open in other areas (Robinson, Noble and Carr 1980).

Public supply and industrial wells completed in the USA near Camas, Washougal, and Vancouver have maximum yields between 1,000 and 6,000 gallons per minute (gpm) with less than 10 feet of drawdown (Mundorff 1964). Wells completed in the fine-grained facies are less productive than wells in the more productive coarse-grained facies of the catastrophic flood deposits.

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<sup>4</sup> This rationale was used to limit the study area to contain only the USA and TGA.

1 Mundorff (1964) estimated that the transmissivity portion of the USA ranged from 1.9  
2 million to 3.5 million gallons per day per foot (gpd/ft).<sup>5</sup> The calculated transmissivities  
3 for City of Vancouver Water Stations WS-1, WS-3 and WS-4, all producing from the  
4 USA, were 2 million gpd/ft, 878,900 gpd/ft, and 586,000 gpd/ft, respectively (Robinson,  
5 Noble and Carr 1980).

6 Based on a review of transmissivities calculated for the City of Vancouver water stations  
7 and transmissivities estimated from reported pump test yields and drawdown (i.e.,  
8 specific capacity), Swanson (1995) assigned a hydraulic conductivity of 1,000 feet/day to  
9 the USA in the Portland Basin. McFarland and Morgan (1996) estimated a median  
10 hydraulic conductivity for the USA of 200 feet/day, with a range of 0.03 to 70,000  
11 feet/day.

12 The transition to the Pleistocene-aged Troutdale Formation is primarily based on a drop  
13 in permeability, followed by harder drilling conditions that were encountered and/or  
14 where cementation or a silty sandy matrix was encountered.

#### 15 **TGA**

16 The TGA underlies the catastrophic flood deposits and alluvial deposits that make up the  
17 USA in the study area. The TGA is composed of partially cemented sandy conglomerate.

18 The elevation of the top of the Troutdale Formation varies noticeably due to an erosional  
19 period prior to the deposition of the catastrophic flood deposits and erosion that occurred  
20 during the flood events. It has been observed that where the upper Troutdale Formation  
21 has been severely weathered, a thick clayey soil may have developed in areas, thus  
22 creating a discontinuous confining unit between the two aquifers (Swanson et al. 1993,  
23 PGG 2002).

24 The permeability and the transmissivity of the TGA have been noted to be at least an  
25 order of magnitude lower than the USA (McFarland and Morgan 1996; PGG 2002). This  
26 difference in permeability and transmissivity is due to the presence of more fines in the  
27 Troutdale Formation, along with lithification and cementation, which ranges from  
28 consolidated to semi-consolidated. Although the TGA contains zones of significant  
29 cementation, it is sufficiently conductive to produce high yield wells. Wells completed in  
30 the TGA commonly yields up to 1,000 gpm (Swanson et al. 1993). The TGA has  
31 historically served as the most productive aquifer in the Salmon Creek basin.

32 Based on limited data, Robinson, Noble, and Ellis (1980) estimated that the  
33 transmissivity of the TGA ranges from about 5,000 to 20,000 gpd/ft in the South Clark  
34 County area. McFarland and Morgan (1996) estimated a median hydraulic conductivity of  
35 the TGA of about 7 feet/day.

36 Exhibit 3-4 shows cross-section orientation lines for selected wells near the study area.  
37 Hydrogeologic unit cross sections are presented in Exhibit 3-5 through Exhibit 3-7.

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<sup>5</sup> Transmissivity is the rate in which water travels through an aquifer of unit width under a unit hydraulic gradient. It is the function of the liquid, porous media and its thickness.



1 **3.7.2 Groundwater Flow**

2 **Recharge and Discharge Areas**

3 Recharge to the USA and TGA occurs from precipitation, and infiltration from rivers,  
4 streams, and stormwater. The principal recharge areas for groundwater in the USA and  
5 TGA are the upland areas of the western Cascade Mountains east of the study area  
6 (Exhibit 1-1). The combined average recharge rate is estimated to be about 22 inches/year  
7 (Snyder et al. 1994) for the Portland Basin. The highest rates (49 inches/year) occur in  
8 the Cascade Range, and the lowest rates (near zero inches/year) at the Columbia and  
9 Willamette Rivers. Seasonal fluctuations in groundwater elevations increase the aquifer  
10 saturated thickness during heavy spring and winter precipitation. As such, the depth to  
11 static water level is greater in the summer and fall months from low precipitation.

12 Groundwater within the USA and TGA likely discharges to the Columbia River, water  
13 supply wells, or infiltrates into the lower sedimentary subsystem. The portion of Clark  
14 County that drains directly to the Columbia River is known as the Columbia Slope  
15 watershed. This 25-square-mile watershed consists of a narrow band of hillsides between  
16 downtown Vancouver and Lacamas Creek. Its northern boundary generally follows Mill  
17 Plain Boulevard and hilltops in Camas, Washington. Except for some wetlands, parks,  
18 and steep hills, most of the area is urbanized.

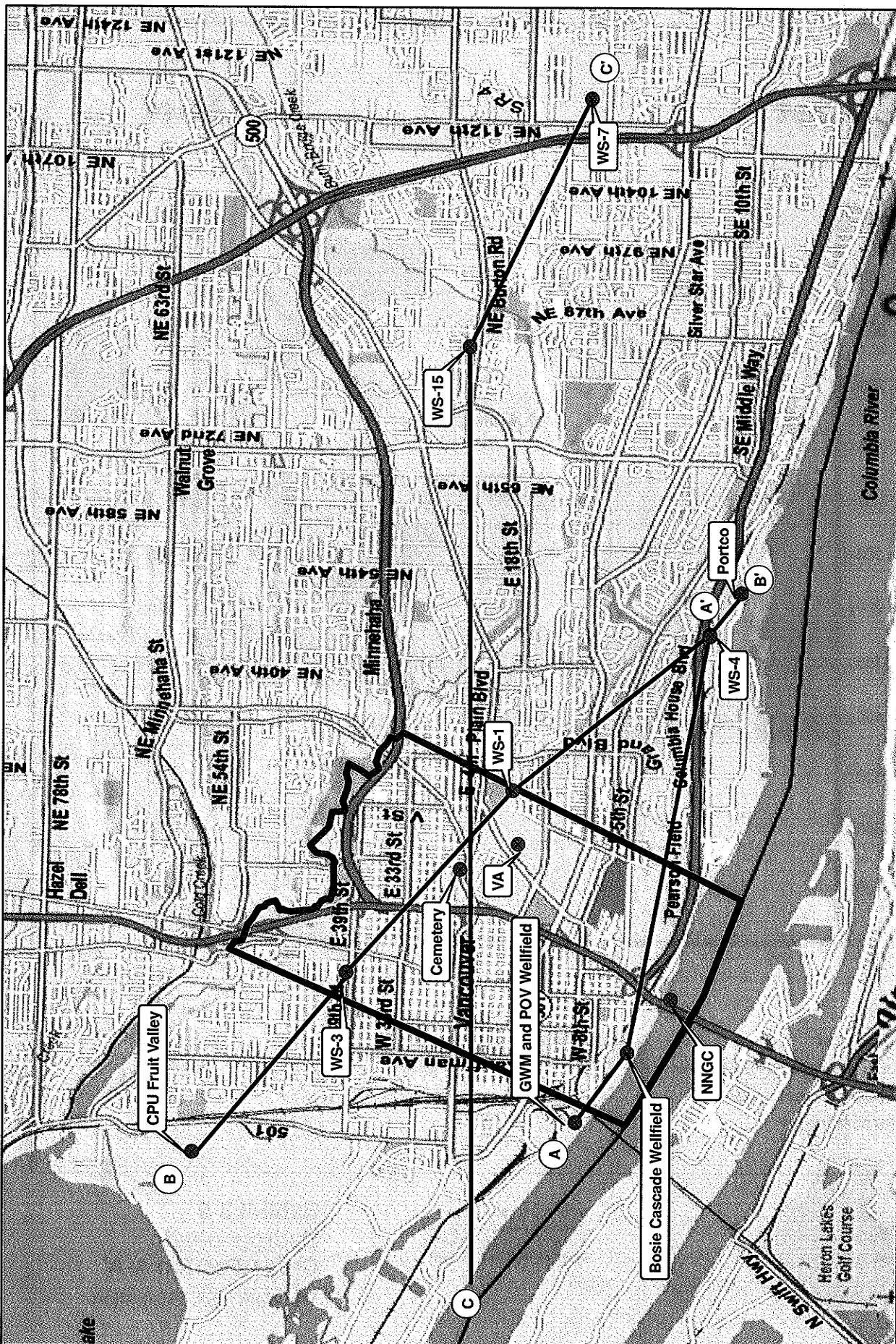
19 **Flow Direction and Gradient**

20 Groundwater in the USA generally flows from recharge areas located northeast of the  
21 study area at elevations about 250 feet above mean sea level (msl) to the southwest  
22 (Exhibit 3-8). The movement of groundwater is controlled by topography, river levels,  
23 and supply well pumping. Within the study area, groundwater elevations are typically 50  
24 feet msl just south of the Burnt Bridge Creek drainage and decrease to approximately 20  
25 feet msl at the Columbia River.<sup>6</sup> Water level elevations sharply increase north of Burnt  
26 Bridge Creek drainage to approximately 150 feet msl. The large observed drop in  
27 groundwater levels south of Burnt Bridge Creek suggests that a low permeability  
28 conditions exists in the area of the creek. This lower permeability condition functions to  
29 reduce the volume of groundwater recharge to the area south of Burnt Bridge Creek.  
30 These physical attributes establish the northern boundary of the study area. Based on the  
31 hydraulically upgradient position, construction activities would not likely impact  
32 groundwater north of this boundary. Further details on groundwater levels within the  
33 study area are displayed on Exhibit 3-9.<sup>7</sup> The exhibit displays the estimated depth to  
34 groundwater below ground surface for May 1995 using 10-foot contour intervals.




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<sup>6</sup> Based on water levels collected during the spring of 1988 (McFarland and Morgan 1996).

<sup>7</sup> Clark County, GIS data layer, No. 1592



**Exhibit 3-4: Cross Section Orientation Map**  
 Troutdale SSA Evaluation

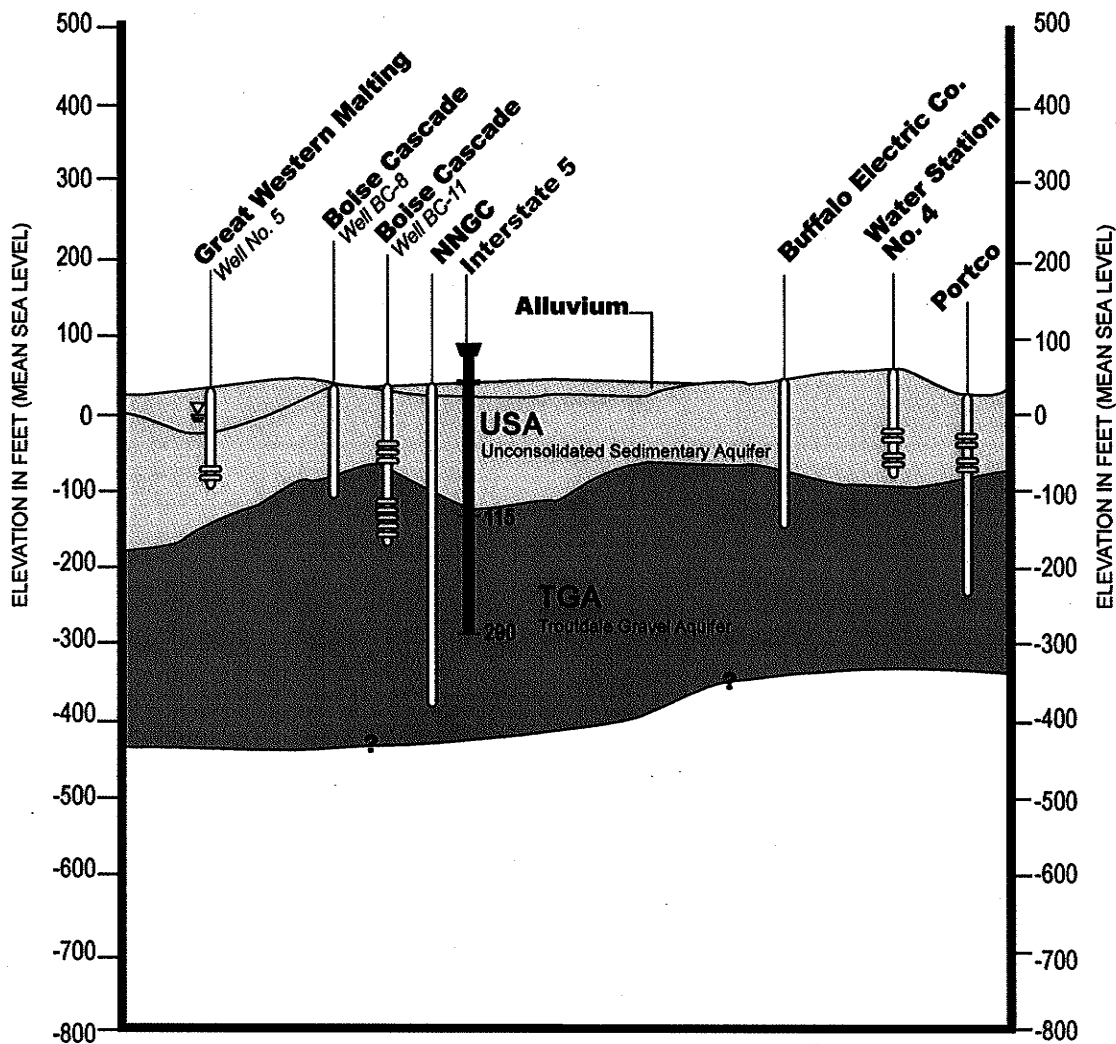
-  Study Area
-  Cross Section Lines
-  Well Locations



Columbia River  
 CROSSING

**A West**

**A' East**



**Legend**

- Borehole/Well
- Approximate Ground Surface Elevation
- Approximate Water Level Elevation
- Well Screen Interval

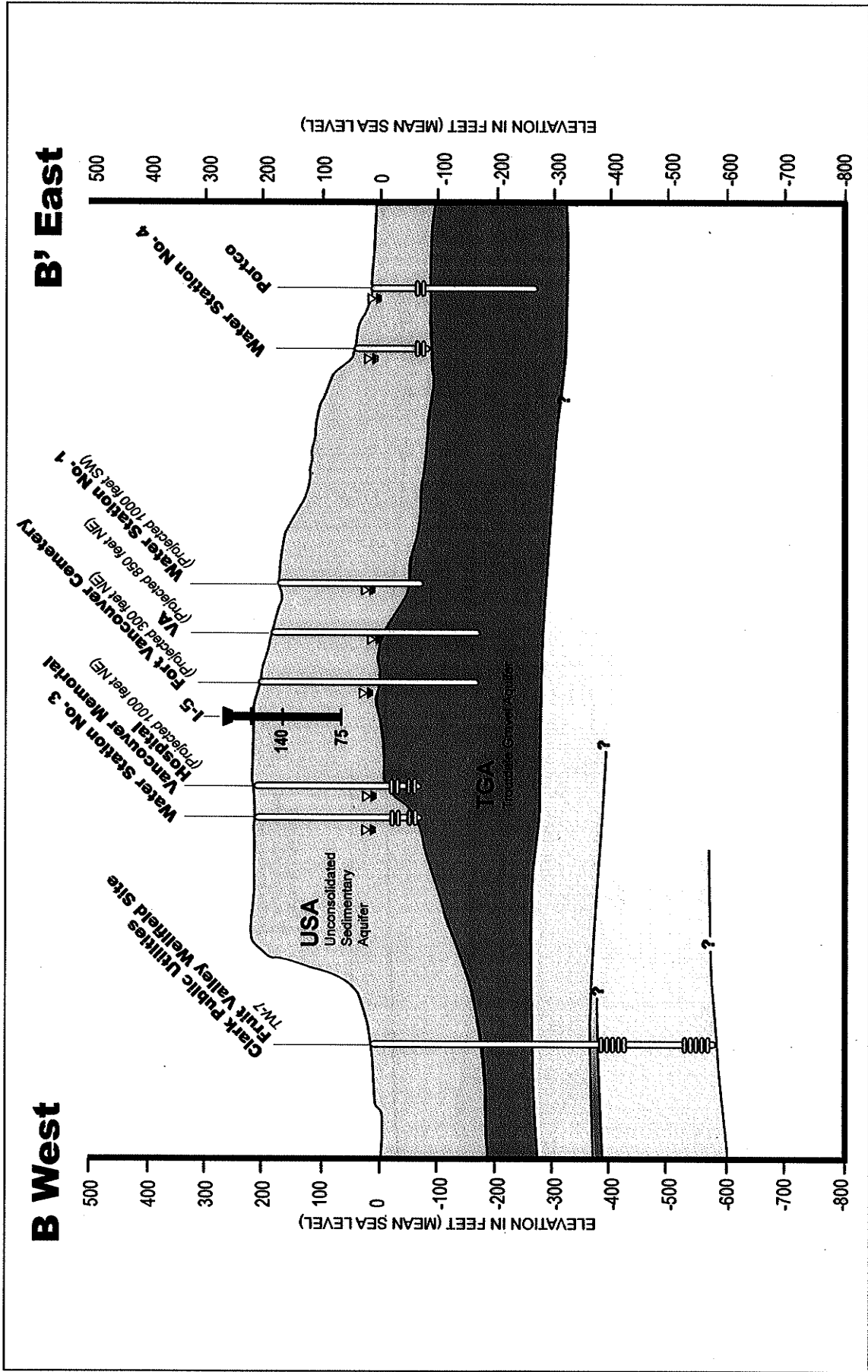
Estimated pile/shaft depths for bridge  
Approximate pile tip elevation -115 to -290 feet

Approximate Vertical  
0 100 200  
0 2,000 4,000  
Approximate Horizontal  
SCALE IN FEET

MODIFIED FROM:  
Pacific Groundwater Group, 2002.  
Evaluation of Clark Public Utilities  
Proposed South Lake Wellfield

**Exhibit 3-5**  
**Hydrogeologic**  
**Cross Section A-A'**  
Trousdale SSA Evaluation



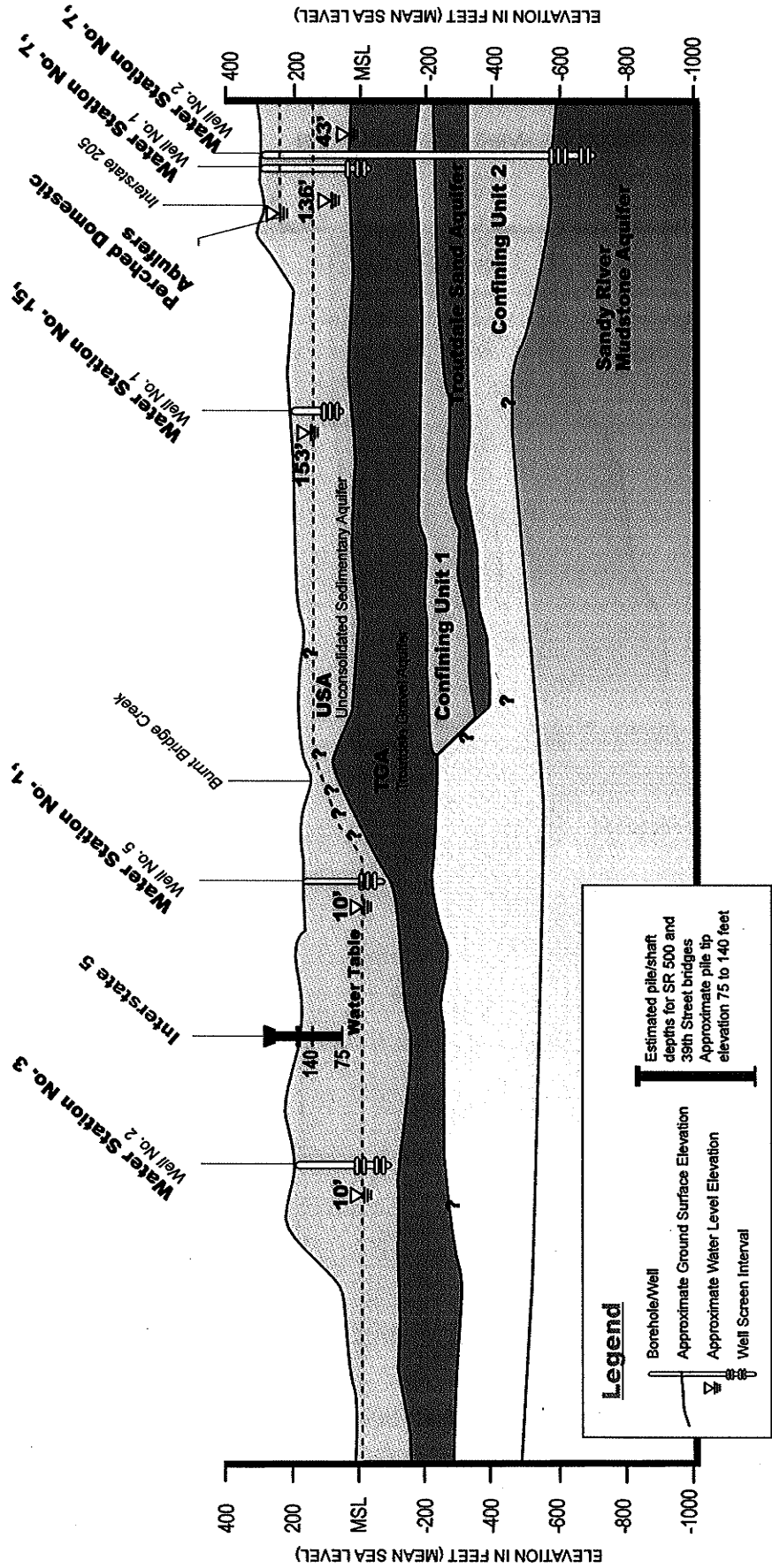


**Exhibit 3-6**  
**Hydrogeologic**  
**Cross Section B-B'**  
 Troutdale SSA Evaluation

MODIFIED FROM:  
 Pacific Groundwater Group, 2002.  
 Evaluation of Clark Public Utilities  
 Proposed South Lake Wetfield

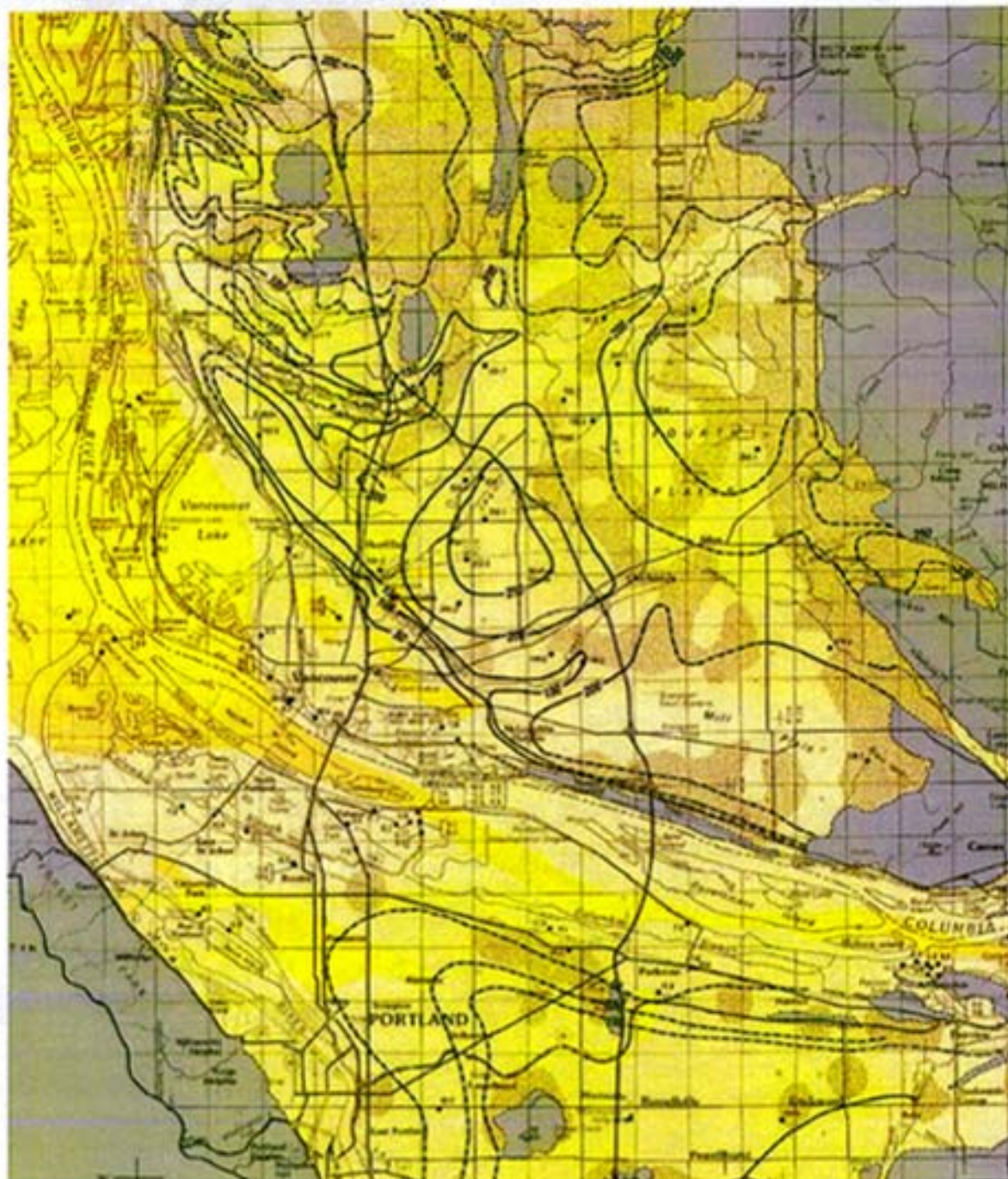
**C West**

**C' East**





**MODIFIED FROM:**  
 Clark County Water Quality Division, 1994, Method to Evaluate Aquifer Vulnerability Through Conjunctive use of a Groundwater Flow Model and Geographic Information System.  
 Robinson & Noble, Inc., 1992, Investigation of the Sandy River Mudstone Aquifer, City of Vancouver.  
 Robinson, Noble & Carr, Inc., 1980, City of Vancouver Groundwater Source and Use Study, Volume 1 Summary.  
 Gray & Osborne, Inc., 1986, Water System Comprehensive Plan, City of Vancouver, November 1986.  
 HDR Engineering, Inc. 2006 Water System Comprehensive Plan, Draft March 2006.

**Exhibit 3-7  
 Hydrogeologic  
 Cross Section C-C'  
 Troutdale SSA Evaluation**



**Legend**

- 
 GROUNDWATER LEVEL CONTOUR. Shows altitude, in feet, of groundwater level, Spring 1988, in the unconsolidated sedimentary aquifer. Dashed where approximate. Contour is variable. Datum is sea level.
- 
 FIELD LOCATED WELL. Completed in the USA. Number is altitude in feet above sea level.



Source:  
 McFarland, W.D. and Morgan, D.S. 1996  
 Description of Ground-Water Flow System in the  
 Portland Basin, Oregon and Washington  
 U.S. Geological Survey Water Supply Paper 2470-A

**Exhibit 3-8**  
**Groundwater Level**  
**Contour Map**  
**USA, Spring 1988**  
 Troutdale SSA Evaluation





Data source:  
Clark County GIS  
Layer Name: GWdepth  
Layer docID: 1592

**Exhibit 3-9: Depth to Groundwater Level Contour Map**  
May 1995  
Troutdale SSA Evaluation



1 Under natural conditions groundwater flow direction of the USA and TGA in the  
2 Vancouver area is to the south southwest. However, this flow condition does not consider  
3 influences from pumping on groundwater flow within the study area.

#### 4 **Influence from Pumping**

5 Groundwater flow in Vancouver area is dominated by the operation of large production  
6 wells primarily at City of Vancouver Water Stations WS-1 and WS-3, the Port of  
7 Vancouver (POV) GPTI well, and Great Western Malting Company supply wells No. 4  
8 and No. 5 (Exhibit 3-10).

9 Extraction rates for city water supply wells vary seasonally based on user demands.  
10 Water demands on the system are highest during the summer and lowest during winter  
11 months (HDR 2006). The average daily production in 2005 for WS-1 was 5.9 million  
12 gallons per day (mgd), and for WS-3 was 3.4 mgd (HDR 2006).

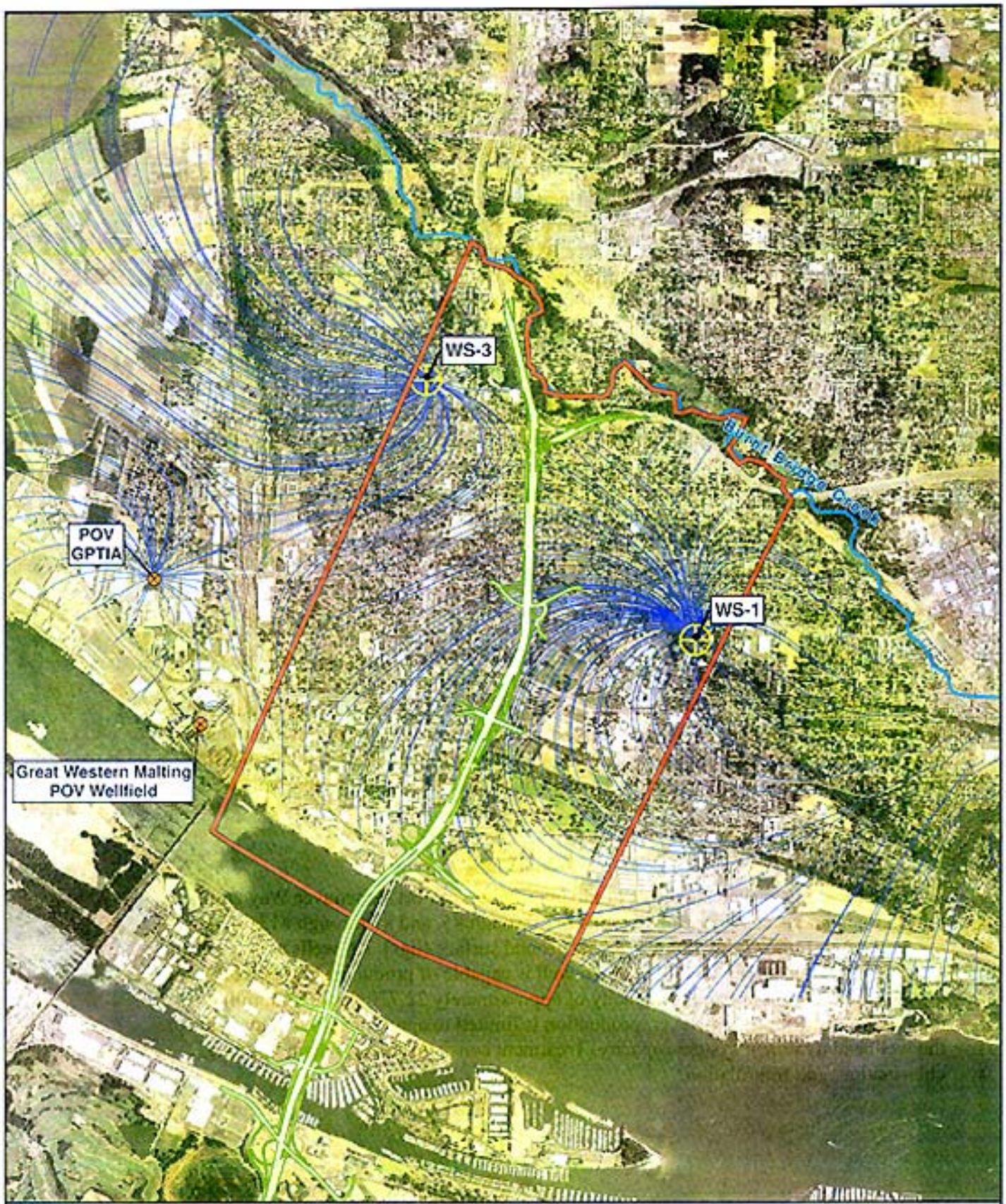
13 Great Western Malting, Inc. process water supply wells No. 4 and No. 5 influence  
14 groundwater flow in the western portion of downtown Vancouver. The wells are also  
15 being utilized by the Port of Vancouver to help contain and capture a chlorinated solvent  
16 plume stemming from the former Swan Manufacturing Company and Cadet  
17 Manufacturing sites. As such, Great Western Malting has been extracting water at a  
18 higher capacity than necessary for plant operations as requested by the Washington State  
19 Department of Ecology (Ecology) and the Port. Production wells—No. 4 and No. 5—  
20 pump at an average combined rate of 3,200 gpm (4.6 mgd). However, the production  
21 rates of these wells will be reduced to a total rate of approximately 900 gpm (1.3 mgd)  
22 when the Port implements its interim action (GPTIA). The GPTIA began operation in  
23 June 2009. The GPTIA well has been designed and constructed to produce an average of  
24 3.6 mgd from the USA.

25 Design and placement of the GPTIA well is based on a groundwater flow model  
26 developed through a combined effort completed on behalf of the Port and Clark Public  
27 Utilities (CPU) (Parametrix, S.S. Papadopoulos et al. 2008). The model was also  
28 developed to help evaluate the performance of the GPTIA well and evaluate the influence  
29 on groundwater flow from CPU's proposed south lake well field. The active area of the  
30 model is bounded by the Columbia River on its southern and western sides, and Burnt  
31 Bridge Creek to the north; it covers approximately 42 square miles including most of the  
32 Vancouver Lake Lowlands and portions of the City of Vancouver that lie west and south  
33 of Interstate 205.

34 Exhibit 3-10 displays model output for groundwater flow lines in the USA (Parametrix  
35 2008). The figure indicates that a majority of the groundwater flow in the downtown  
36 Vancouver area is captured by WS-1, WS-3 and the GPTI well. Simulated groundwater  
37 flow lines have been used to help define the eastern and western boundaries of the study  
38 area (Section 1). Boundaries are necessary to place constraints on the active area in which  
39 the evaluation will be conducted. Specifically, the boundaries are drawn along internal  
40 flow lines that represent hydraulic capture of groundwater movement within the study  
41 area. Or stated another way, a particle of water within the study area will likely be

- 1 retained within the study area and ultimately travel to a well head. Model simulations
- 2 indicate that groundwater within the study area will be captured at a well head within a
- 3 timeframe of 1 to 5 years (Mike Riley, S.S. Papadopoulos, personal communication).





**Exhibit 3-10: Extraction Wells Simulated Flow Path Troutdale SSA Evaluation**



## 1 **Tidal Influence**

2 Water levels in the USA and TGA are influenced by changes in the Columbia River  
3 stage. The level of influence tends to be greatest near the river, and dissipates inland. In  
4 turn the river stage is influenced by tidal fluctuations and upstream dam releases  
5 (Parametrix, Papadopulos et al. 2008). The rapid response between changes in river stage  
6 and corresponding changes in groundwater levels indicates a high interconnectivity  
7 between the river, the USA, and the upper portion of the TGA. Groundwater table  
8 fluctuations due to river stage changes are less significant with increasing distance from  
9 the Columbia River.

### 10 **3.7.3 Beneficial Groundwater Use**

11 Groundwater within the TSSA has a variety of beneficial uses. These uses include  
12 drinking water for consumption, irrigation water for agriculture, and process and cooling  
13 water for industrial use. The TSSA is a suitable source for these beneficial uses due to its  
14 high water quality, accessibility, and overall capacity. Well head locations for  
15 approximately 36 wells<sup>8</sup> located within ½ mile of the LPA are displayed in Exhibit 3-11.  
16 Utilization of the TSSA in the study area includes industrial wells for heat exchange,  
17 irrigation wells, industrial-process water wells, and drinks water supply wells.

### 18 **City of Vancouver Municipal Well Fields**

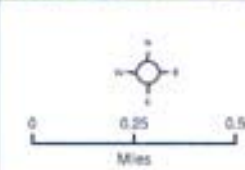
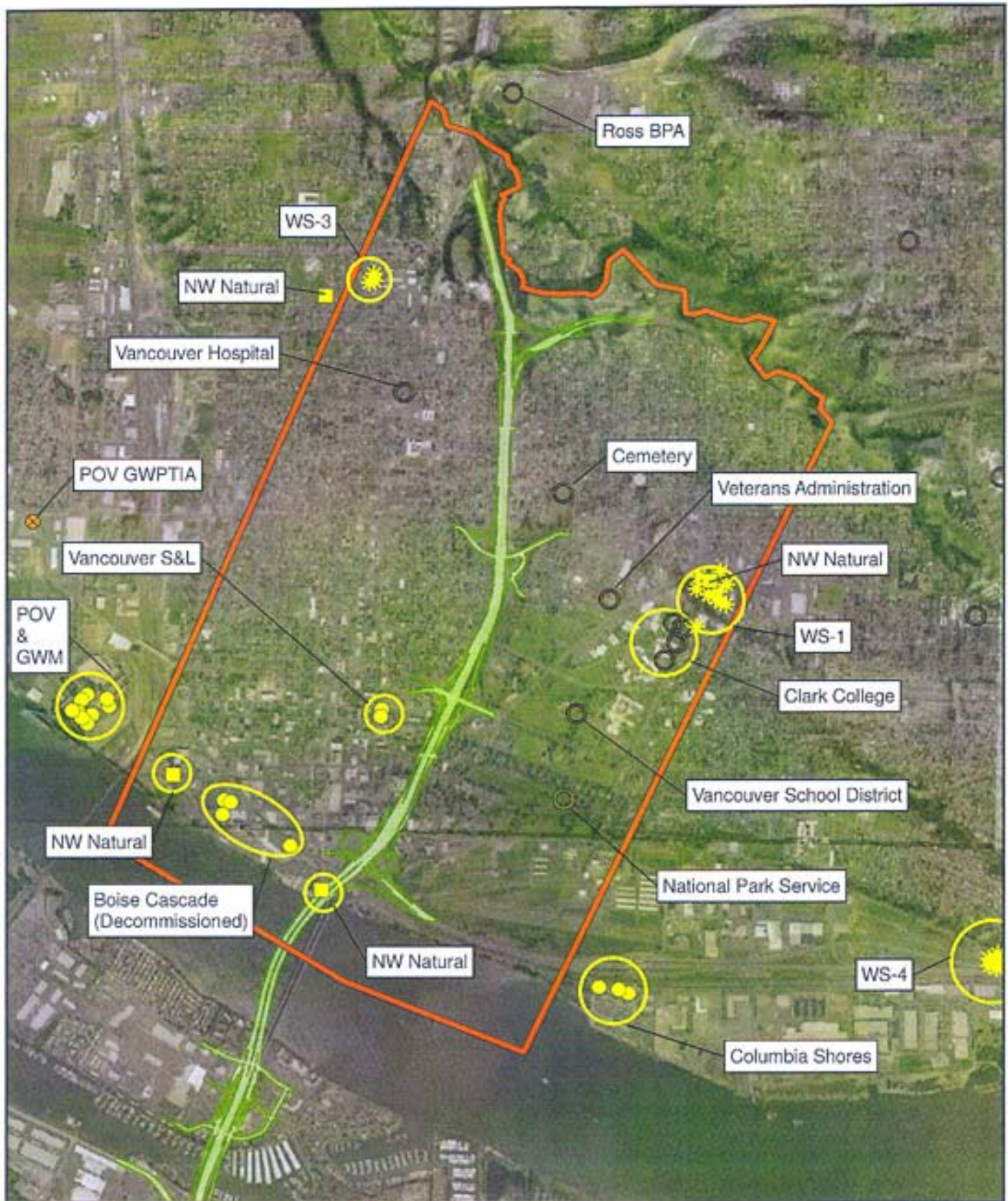
19 The City of Vancouver (City) pumps an average of 26 mgd from the TSSA, with peak  
20 demands up to approximately 53 mgd in 2003 (HDR 2006). The City extracts  
21 groundwater from 16 water stations, each with several production wells. Based on the  
22 anticipated population growth for the City, demand on the water system is estimated to  
23 increase between 61 and 71 mgd by 2012, and between 74 and 90 mgd by 2026 (HDR  
24 2006). These increases in demand will add additional stress to the aquifer. New well  
25 heads will likely be added to WS-1.

### 26 **WS-1**

27 Water Station 1 is located southeast of the intersection of Fort Vancouver Way and E.  
28 Fourth Plain and is composed of 12 wells (#1 through #5, and #7 through #13). The wells  
29 range in depth from 235 to 280 feet below ground surface (bgs). All wells at this water  
30 station extract water from the USA. Each well is capable of producing between 900 and  
31 2,800 gpm, for a total pumping capacity of approximately 22,770 gpm (33.3 million  
32 gallons per day [mgd]). However, production is limited to approximately 27 mgd due to  
33 the wellhead treatment system capacity. Treatment consists of aeration/air stripping,  
34 chlorination, and fluoridation.

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<sup>8</sup> These data were mapped by the USGS in the 1980s. These data have not been field checked. These points are out of date and incomplete but are the "best available" source of well information.



- Groundwater Remediation Well
- ☀ Well Exchange Well
- Process Water
- Ingestion
- Municipal
- Well Field
- Study Area

**Exhibit 3-11: Groundwater Beneficial Use Locations**  
 Troutdale SSA Evaluation



1 In 1989, the City and EPA began a sampling program to identify the source of PCE near  
2 WS-1. A soil-gas survey collected 19 soil-gas samples in the vicinity of WS-1. Five  
3 private wells were selected for the collection of groundwater samples within a 1-mile  
4 radius of WS-1. The source of PCE in groundwater was not determined. Although the  
5 source of PCE was not identified, EPA determined that the remedial action for the  
6 dissolved phase plume would be pump and treat. To remove PCE from the water supply,  
7 five air stripping towers were installed in 1993. In June 1994, EPA officially placed WS-  
8 1 on the NPL.

### 9 **WS-3**

10 Water Station 3 is located northwest of NW 42nd Street and NW Washington Street and  
11 is composed of three wells (#1 through #3). The wells range in depth from 259 to 275  
12 feet bgs. All wells at this water station extract water from the USA. Each well has a  
13 pumping capacity of approximately 2,000 gpm, or a total pumping capacity of 5,800 gpm  
14 (8.9 mgd). This water station capacity is limited to 8.6 mgd due to water rights. All wells  
15 at this water station extract water from the USA. Water at the well head is treated by  
16 chlorination and fluoridation.

### 17 **Boise Cascade**

18 The Boise Cascade site contained several production wells for process water. According  
19 to the Ecology well logs for the site, the wells have been decommissioned in place by  
20 filling with cement grout.

### 21 **Port of Vancouver**

22 The Port of Vancouver has installed a large-diameter extraction well (GPTIA well) in the  
23 vicinity of the suspected source area of chlorinated solvent plume. The well is part of an  
24 interim remedial action effort to hydraulically contain source area contaminants. The  
25 GPTIA well has a pumping capacity of approximately 2,500 gpm. All water is treated  
26 using a combined carbon / aeration system prior to the water discharged to the Columbia  
27 River.

### 28 **Great Western Malting**

29 Great Western Malting (a.k.a. ConAgra Malt) currently operates two extraction wells,  
30 No. 4 and No. 5. Groundwater from the wells is treated using an air stripper tower.  
31 Treated water is used germination of malt and as process water for cooling. The wells are  
32 capable of producing 4,000 gpm, but are currently extracting water at a combined rate of  
33 3,200 gpm.

### 34 **3.7.4 Critical Aquifer Recharge Area Designation**

35 The City of Vancouver relies entirely on the groundwater extracted from the TSSA for its  
36 drinking water supply. Prior to the EPA's designation of the Troutdale Aquifer System as  
37 an TSSA, the City of Vancouver recognized its dependence on the aquifer and the  
38 importance of protecting the resource. The City of Vancouver has designated the entire



1 area within the city boundaries as a Critical Aquifer Recharge Area as specified the  
2 Water Resources Protection Ordinance VMC Title 14 Section 26, dated 2002. The  
3 ordinance requires minimum standards to protect critical aquifer, establishes compliance  
4 standards for business and industry to manage hazardous materials, and creates special  
5 protection areas around city well heads. Special protection areas are defined as areas that  
6 are 1,900 radial feet from any municipal water supply well. As such the city applies  
7 development restrictions to activities inside the special protection areas pursuant VM  
8 14.26.135. These restrictions mainly address Class I and II Operations, septic systems,  
9 and infiltration systems.

### 10 **3.7.5 Groundwater Quality**

11 Contaminants from historic commercial and industrial activities within the City of  
12 Vancouver have resulted in diminishing groundwater quality. Exhibit 3-12 displays  
13 posted contaminant concentrations observed in the TSSA based on communications with  
14 Ecology site managers. The exhibit indicates that contaminants such as chlorinated  
15 ethenes, petroleum products, and metals are found in groundwater throughout the study  
16 area.<sup>9</sup>

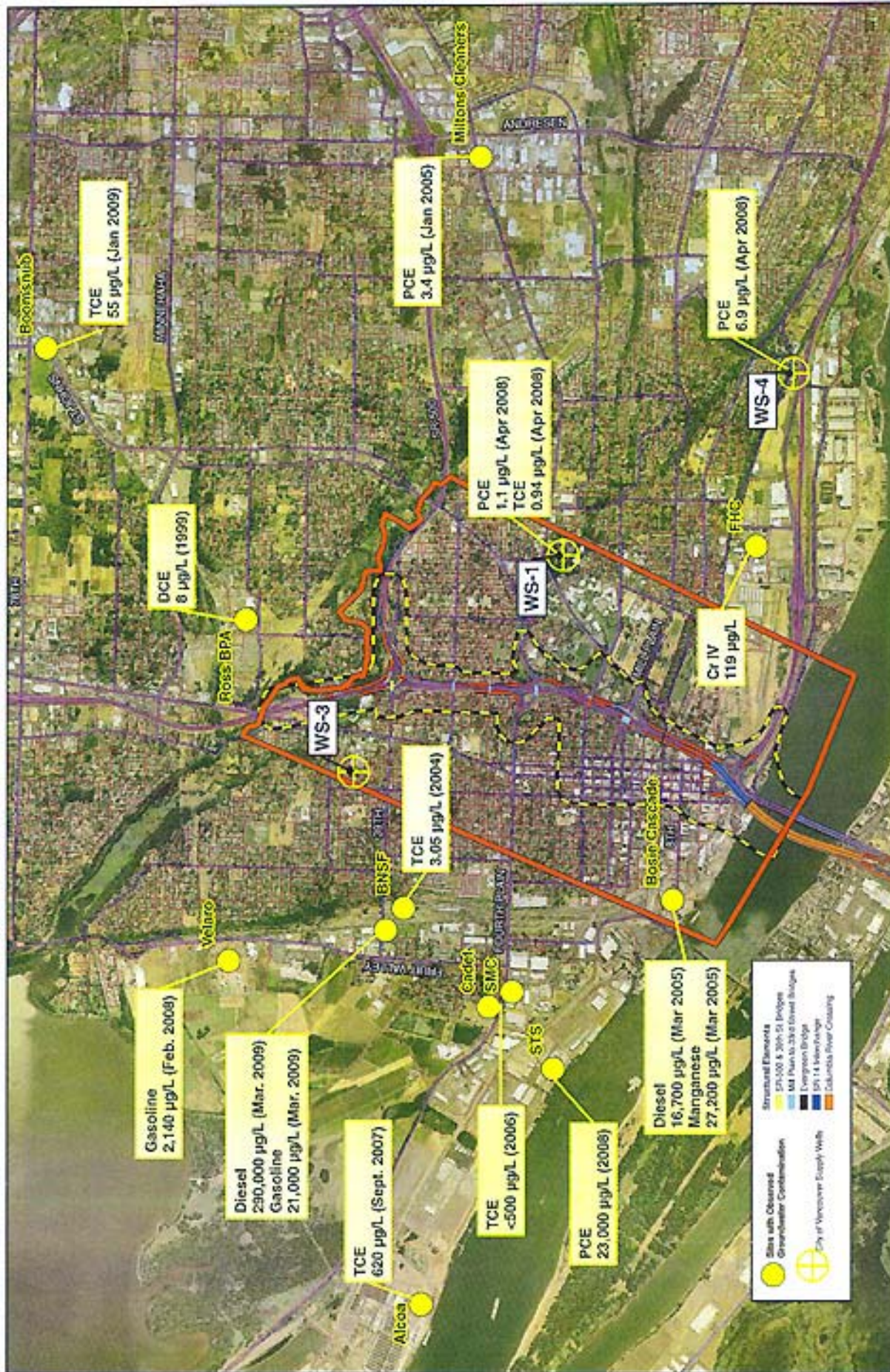
17 As stipulated in the Safe Drinking Water Act (SDWA) and Washington Administrative  
18 Code (WAC) Chapter 290, suppliers of drinking water must monitor for and meet  
19 primary and secondary drinking water standards. From approximately January 1979 to  
20 October 2008, the City of Vancouver has sampled and analyzed groundwater from it WS  
21 for the following classes of compounds: inorganics, volatile organic compounds (VOCs),  
22 herbicides, pesticides, insecticides, radionuclides, fumigants, dioxins, and nitrate.  
23 Analytical results for WS-1 and WS-3 are tabulated at  
24 <http://www4.doh.wa.gov/SentryInternet/SingleSystemViews/SamplesSingleSys.aspx>

25 Review of water quality data by the Washington State Department of Health indicates  
26 that no analytes have been detected at or above their respective maximum contaminant  
27 limit (MCL) or secondary maximum contaminant limit (SMCL) in groundwater at WS-1,  
28 except for tetrachloroethene (PCE) at 9.2 micrograms per liter [ $\mu\text{g/L}$ ] (MCL = 5  $\mu\text{g/L}$ ) in  
29 September 1999. However, no exceedance in drinking water standards has been  
30 documented in the last 5 years. The most recent available analytical results indicate that  
31 PCE and TCE were detected at 1.1  $\mu\text{g/L}$  and 0.94  $\mu\text{g/L}$  at WS-1 in April 2008.

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<sup>9</sup> No comprehensive study that describes the distribution of contaminants in groundwater for the Vancouver Area is available. Contaminant information was obtained from Ecology Site Managers to help graphically display generalized contaminant impacts.





**Exhibit 3-12: Summary of General Contaminant Concentrations in Groundwater Troutdale SSA Evaluation**

Columbia River  
**CROSSING**

**UNITS**  
µg/L=Micrograms per liter

**ACRONYMS**  
PCE=Trichloroethene  
TCE=Trichloroethene  
DCE=Dichloroethene  
CR(IV)=Chromium(IV)

**NOTES:** Contaminant concentrations are based on communications with Ecology site managers, July 2009.  
Noted constituent represents a site specific risk driver.

